## Application Note

# Measuring Temperature Using a Thermocouple 

By: M. Ganesh Raaja<br>Associated Project: Yes Associated Part Family:CY8C26xxx<br>PSoC Designer Version: 4.00<br>Associated Application Notes: AN2099, AN2038, AN2101

## Summary

This Application Note explains how to measure temperature using a J Type Thermocouple with a PSoC. Following the principle, any thermocouple input can be measured.

## Introduction

Thermocouples are widely used in industrial applications for the following reasons:

- They are robust
- They measure over a wide range ( $-270^{\circ}$ to $3000^{\circ} \mathrm{C}$ )
- They are available in a wide variety of packages and probes


## Thermocouple Principle

A thermocouple consists of two pieces of dissimilar metals in the form of wire fused at one end. This is called the hot junction. The other end is connected to a measuring circuit. This is called the cold junction. The difference in temperature between the hot and cold junctions causes an EMF to develop. This EMF can be measured by the measuring circuit.

Because the thermocouple is a reference device, the absolute temperature (hot junction) can be measured only if the reference (cold junction) is known. The reference temperature is called the Cold Junction Temperature. Adding the thermocouple equivalent EMF of this temperature to the one measured from the thermocouple is called Cold Junction Compensation.

There are different types of thermocouples such as J, K, T, R, and S just to name a few. Each type has its own temperature coefficient and range of measurement.

The output of the thermocouple is not linear throughout the measurement range.

There are two methods that can be used to acquire an accurate temperature. Using a multiorder polynomial equation (Equation 1), the temperature can be calculated accurately as close as $+0.02^{\circ} \mathrm{C}$.

$$
\mathrm{T}=\left(\mathrm{a}_{0}+\mathrm{a}_{1} \mathrm{~V}+\mathrm{a}_{2} \mathrm{~V}^{2}+\ldots+\mathrm{a}_{\mathrm{n}} \mathrm{~V}^{\mathrm{n}}\right) \text { Equation } 1
$$

The polynomial coefficients for different types of thermocouples can be found in Table-3 in the Appendix.

This method is quite complicated and involves high precision mathematics, which heavily taxes the resources of an 8-bit device.

The second method is the use of lookup tables. Here, we divide the whole measurement range of the thermocouple into many regions and identify the coefficient for each region. The higher the number of regions, the better the accuracy. We will use this method in this Application Note.

## Steps Involved

The whole process can be broken into the following steps.

1. Find Cold Junction Temperature and thermocouple voltage corresponding to that temperature. This is the Cold Junction Compensation voltage.
2. Measure thermocouple voltage.
3. Add the Cold Junction Compensation voltage to the thermocouple voltage.
4. Find coefficient.
5. Find temperature.

## 1. Find Cold Junction Compensation:

Many circuits can be used to measure the reference temperature; Thermistor, RTD, and Diode come to mind.

In this circuit, the LM335 Precision Temperature Sensor is used to sense the Cold Junction Temperature. This IC has a linear output of 10 $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ and can give excellent accuracy without any calibration. The output of this IC is 0 V at absolute zero $\left(0^{\circ} \mathrm{K}\right)$. At $0^{\circ} \mathrm{C}$, the output voltage is $2.7315 \mathrm{~V}\left(273.15^{\circ} \mathrm{K}\right)$. The LM335 output is connected to P2[1], so that it can be directly configured as an ADC input without using any Continuous Time analog PSoC blocks.

A diode can also be used to sense room temperature. Any common diode like 1N4148 can be used. A diode exhibits a temperature coefficient of $-2.2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$. A single resistance can be used to set the diode current. But the absolute voltage will have some tolerance and will have to be calibrated.

Correlated Double Sampling (CDS) is performed while measuring Cold Junction Temperature. CDS is explained in step \#2. First, the ADC input is shorted to AGND and the output measured. The LM335 output is connected to the ADC input and the ADC output is measured. The zero value is subtracted from this value to get an offsetcorrected reading.

Now, considering a 12-bit ADC and full-scale voltage of 1.3 V (REFHI), the following equation gives the LM335 voltage.

$$
\text { V }=(1.3 \mathrm{~V} / 2048) * \text { ADC Count Equation } 2
$$

The LM335 output is at $10 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ which modifies the equation to:

$$
\mathrm{T}=(130 / 2048) * \text { ADC Count Equation } 3
$$

This yields temperature directly (in ${ }^{\circ} \mathrm{K}$ ). As the output of LM 335 at $0^{\circ} \mathrm{C}$ is 2.731 V with reference to VSS, and as ADC measurement is with reference to AGND which is 2.6 V , subtracting 13 from the calculated value will give Cold Junction Temperature directly in ${ }^{\circ} \mathrm{C}$.

From this temperature, find the corresponding thermocouple voltage from table reference (coldJunction[]) in the Appendix.

## 2. Measure Thermocouple Voltage:

The thermocouple input is fed to an INSAMP User Module with a gain of 16. The output of $J$ Type Thermocouple is 69.55 mV at $1200^{\circ} \mathrm{C}$.

The output of the INSAMP is roughly 1.11 V at this temperature. This is fed to an ADCINC12 User Module.

When we have to measure such small voltages, the problems of offset error and signal-to-noise ratio come into consideration. To overcome these problems we will use CDS and Infinite Impulse Response (IIR) filter techniques.

## Correlated Double Sampling (CDS):

This method reduces offset errors present in the signal-conditioning amplifiers and the ADC. The following steps are involved.

1. Short the inputs. Measure ADC output. Store as Zero.
2. Connect inputs to thermocouple. Measure output. Store as Signal.
3. Subtract Zero from Signal.

## Infinite Impulse Response (IIR) Filter:

This is a low-pass filter implemented in software. This averages and effectively reduces the noise from the input signal.

In this application, the IIR filter constant has been set to 4. This results in poor response time but very good noise rejection. Most industrial applications that measure high temperatures do not need fast response time. For faster response, the filter constant can be reduced.

For details on modifying the filter constant and other IIR techniques, see Application Note AN2099 "Single-Pole IIR Filters. To Infinity And Beyond!"

The ADC output after CDS is passed through the low-pass IIR filter. From the output of this filter, the thermocouple voltage can be calculated by the following formula:

$$
\text { volts }=\text { ADC Counts } * \text { Range } / \text { fullScale }
$$

## Equation 4

For calibration purposes, the range is set to 50 mV and fullScale is the ADC Counts when input is 50 mV . For better resolution, ADC Counts is multiplied by 5,000 and divided by fullScale. The resolution of the result is 10 uV /count.

## 3. Cold Junction Compensation:

Add the Cold Junction Compensation voltage calculated in step \#2 to the measured thermocouple voltage to get a cold junction compensated output.

## 4. Find Coefficient:

Let us consider a J Type Thermocouple. The EMF table of J Type Thermocouple can be found in Tables-1 and 2 in the Appendix.

First, we have to build a lookup table from the EMF table of the J Type Thermocouple. Let us divide the whole table into 0.64 mV divisions and identify the coefficient for each division. Compiling them will give us the lookup table.

As resolution of the measured voltage is 10 uV , the coefficient is also calculated for ${ }^{\circ} \mathrm{C} / 10 \mathrm{uV}$. Multiply this fractional number by 10,000 to convert it to an integer.

As the measured voltage is in tens of microvolts, the thermocouple voltage is divided by 64 to get the lookup table offset. Sixty-four has been selected because it is easier to perform the division by rotating the voltage 6 times to the right.

The procedure of building the lookup table can be found in the Excel .xls file attached with the project.

## 5. Find Temperature:

Once the thermocouple voltage and coefficient are known, temperature can be calculated by multiplying the thermocouple voltage by the sensitivity coefficient for that type of thermocouple. Some examples of thermocouple sensitivies are given in Table 1.

## Table 1. Thermocouple Coefficients

| Type | Sensitivity Coefficient |
| :---: | :---: |
| K | $41 \mathrm{uV} /{ }^{\circ} \mathrm{C}$ |
| E | $68 \mathrm{uV} /{ }^{\circ} \mathrm{C}$ |
| R | $10 \mathrm{uV} /{ }^{\circ} \mathrm{C}$ |
| N | $10 \mathrm{uV} /{ }^{\circ} \mathrm{C}$ |

In PSoC Designer, some assembly routines have been written for 16 -bit multiplication and 24 -bit division. These routines are called from C. This is to minimize the time taken in math operations. For details on 16-bit multiplication, refer to Application Note AN2038, and for details on 24bit division, refer to Application Note AN2101.

To support signed division, first the dividend is tested to determine if it is negative. If it is negative, the sign is saved, the value is made positive and division is performed. Then the sign is restored by 2's complementing the result.

## Software

The software consists of three main components.

1. ReadAdc()
2. ProcessAdc()
3. CheckCalibration()

## ReadAdc():

This routine reads from both the thermocouple and LM335, performs CDS and IIR filtering and updates vTc and vColdJunction.

## ProcessAdc():

This routine calculates Cold Junction Temperature from vColdJunction, performs the Cold Junction Compensation on vTc and calculates the temperature after finding the coefficient. It then updates the LCD display with the measured temperature and room temperature.

If the voltage is positive, the coefficient is taken from the positive lookup table. If the voltage is negative, the coefficient is taken from the negative lookup table.

The total time for calculation of temperature and updating the display is 2.7 mS at a CPU speed of 24 MHz .

## CheckCalibration():

This routine performs calibration. A push-button switch connected to P2[3] is used for Full Scale Calibration. Another push button connected to P2[5] is used for Zero Calibration.

When the Zero Calibration switch is pressed, the value of vTc is stored as zero.

When the Full-Scale Calibration switch is pressed, the value of $v T c$ is stored as fullScale.

## Calibration:

Though CDS takes care of the zero offset error, for optimum accuracy, a software zero calibration has been added. This takes care of any residual offset error.

- Apply 0 mV at the thermocouple input
- Wait until the display stabilizes
- Press the Zero Calibration push button
- Apply 50 mV at the thermocouple input
- Wait until the display stabilizes
- Press the Full-Scale Calibration push button

The instrument is now calibrated and accurate to $\pm 2^{\circ} \mathrm{C}$. For test results see Table-4 in the Appendix.

The zero calibration procedure can be omitted if some inaccuracy can be tolerated. In this case, the error can go up to $\pm 4^{\circ} \mathrm{C}$.

## Conclusion

Using the described method, temperature can be measured for any thermocouple input. As there are minimal external components, a low-cost temperature controller can be built using a PSoC, and adding some keys, a 4-digit LED display, and one or two relay outputs. The controller can be designed to measure various thermocouples like J, K, R, T, etc. A feature can be implemented to select the thermocouple and program the set point using the front panel keys.

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## APPENDIX

Table 1. J Type Thermocouple EMF Table for +ve Temperatures (in mV)

| ${ }^{\circ} \mathrm{C}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.000 | 0.050 | 0.101 | 0.151 | 0.202 | 0.253 | 0.303 | 0.354 | 0.405 | 0.456 |
| 10 | 0.507 | 0.558 | 0.609 | 0.660 | 0.711 | 0.762 | 0.814 | 0.865 | 0.916 | 0.968 |
| 20 | 1.019 | 1.071 | 1.122 | 1.174 | 1.226 | 1.277 | 1.329 | 1.381 | 1.433 | 1.485 |
| 30 | 1.537 | 1.589 | 1.641 | 1.693 | 1.745 | 1.797 | 1.849 | 1.902 | 1.954 | 2.006 |
| 40 | 2.059 | 2.111 | 2.164 | 2.216 | 2.269 | 2.322 | 2.374 | 2.427 | 2.480 | 2.532 |
| 50 | 2.585 | 2.638 | 2.691 | 2.744 | 2.797 | 2.850 | 2.903 | 2.956 | 3.009 | 3.062 |
| 60 | 3.116 | 3.169 | 3.222 | 3.275 | 3.329 | 3.382 | 3.436 | 3.489 | 3.543 | 3.596 |
| 70 | 3.650 | 3.703 | 3.757 | 3.810 | 3.864 | 3.918 | 3.971 | 4.025 | 4.079 | 4.133 |
| 80 | 4.187 | 4.240 | 4.294 | 4.348 | 4.402 | 4.456 | 4.510 | 4.564 | 4.618 | 4.672 |
| 90 | 4.726 | 4.781 | 4.835 | 4.889 | 4.943 | 4.997 | 5.052 | 5.106 | 5.160 | 5.215 |
| 100 | 5.269 | 5.323 | 5.378 | 5.432 | 5.487 | 5.541 | 5.595 | 5.650 | 5.705 | 5.759 |
| 110 | 5.814 | 5.868 | 5.923 | 5.977 | 6.032 | 6.087 | 6.141 | 6.196 | 6.251 | 6.306 |
| 120 | 6.360 | 6.415 | 6.470 | 6.525 | 6.579 | 6.634 | 6.689 | 6.744 | 6.799 | 6.854 |
| 130 | 6.909 | 6.964 | 7.019 | 7.074 | 7.129 | 7.184 | 7.239 | 7.294 | 7.349 | 7.404 |
| 140 | 7.459 | 7.514 | 7.569 | 7.624 | 7.679 | 7.734 | 7.789 | 7.844 | 7.900 | 7.955 |
| 150 | 8.010 | 8.065 | 8.120 | 8.175 | 8.231 | 8.286 | 8.341 | 8.396 | 8.452 | 8.507 |
| 160 | 8.562 | 8.618 | 8.673 | 8.728 | 8.783 | 8.839 | 8.894 | 8.949 | 9.005 | 9.060 |
| 170 | 9.115 | 9.171 | 9.226 | 9.282 | 9.337 | 9.392 | 9.448 | 9.503 | 9.559 | 9.614 |
| 180 | 9.669 | 9.725 | 9.780 | 9.836 | 9.891 | 9.947 | 10.002 | 10.057 | 10.113 | 10.168 |
| 190 | 10.224 | 10.279 | 10.335 | 10.390 | 10.446 | 10.501 | 10.557 | 10.612 | 10.668 | 10.723 |
| 200 | 10.779 | 10.834 | 10.890 | 10.945 | 11.001 | 11.056 | 11.112 | 11.167 | 11.223 | 11.278 |
| 210 | 11.334 | 11.389 | 11.445 | 11.501 | 11.556 | 11.612 | 11.667 | 11.723 | 11.778 | 11.834 |
| 220 | 11.889 | 11.945 | 12.000 | 12.056 | 12.111 | 12.167 | 12.222 | 12.278 | 12.334 | 12.389 |
| 230 | 12.445 | 12.500 | 12.556 | 12.611 | 12.667 | 12.722 | 12.778 | 12.833 | 12.889 | 12.944 |
| 240 | 13.000 | 13.056 | 13.111 | 13.167 | 13.222 | 13.278 | 13.333 | 13.389 | 13.444 | 13.500 |
| 250 | 13.555 | 13.611 | 13.666 | 13.722 | 13.777 | 13.833 | 13.888 | 13.944 | 13.999 | 14.055 |
| 260 | 14.110 | 14.166 | 14.221 | 14.277 | 14.332 | 14.388 | 14.443 | 14.499 | 14.554 | 14.609 |
| 270 | 14.665 | 14.720 | 14.776 | 14.831 | 14.887 | 14.942 | 14.998 | 15.053 | 15.109 | 15.164 |
| 280 | 15.219 | 15.275 | 15.330 | 15.386 | 15.441 | 15.496 | 15.552 | 15.607 | 15.663 | 15.718 |
| 290 | 15.773 | 15.829 | 15.884 | 15.940 | 15.995 | 16.050 | 16.106 | 16.161 | 16.216 | 16.272 |
| 300 | 16.327 | 16.383 | 16.438 | 16.493 | 16.549 | 16.604 | 16.659 | 16.715 | 16.770 | 16.825 |
| 310 | 16.881 | 16.936 | 16.991 | 17.046 | 17.102 | 17.157 | 17.212 | 17.268 | 17.323 | 17.378 |
| 320 | 17.434 | 17.489 | 17.544 | 17.599 | 17.655 | 17.710 | 17.765 | 17.820 | 17.876 | 17.931 |
| 330 | 17.986 | 18.041 | 18.097 | 18.152 | 18.207 | 18.262 | 18.318 | 18.373 | 18.428 | 18.483 |
| 340 | 18.538 | 18.594 | 18.649 | 18.704 | 18.759 | 18.814 | 18.870 | 18.925 | 18.980 | 19.035 |
| 350 | 19.09 | 19.146 | 19.201 | 19.256 | 19.311 | 19.366 | 19.422 | 19.477 | 19.532 | 19.587 |
| 360 | 19.642 | 19.697 | 19.753 | 19.808 | 19.863 | 19.918 | 19.973 | 20.028 | 20.083 | 20.139 |
| 370 | 20.194 | 20.249 | 20.304 | 20.359 | 20.414 | 20.469 | 20.525 | 20.58 | 20.635 | 20.69 |
| 380 | 20.745 | 20.8 | 20.855 | 20.911 | 20.966 | 21.021 | 21.076 | 21.131 | 21.186 | 21.241 |
| 390 | 21.297 | 21.352 | 21.407 | 21.462 | 21.517 | 21.572 | 21.627 | 21.683 | 21.738 | 21.793 |
| 400 | 21.848 | 21.903 | 21.958 | 22.014 | 22.069 | 22.124 | 22.179 | 22.234 | 22.289 | 22.345 |
| 410 | 22.4 | 22.455 | 22.51 | 22.565 | 22.62 | 22.676 | 22.731 | 22.786 | 22.841 | 22.896 |
| 420 | 22.952 | 23.007 | 23.062 | 23.117 | 23.172 | 23.228 | 23.283 | 23.338 | 23.393 | 23.449 |
| 430 | 23.504 | 23.559 | 23.614 | 23.67 | 23.725 | 23.78 | 23.835 | 23.891 | 23.946 | 24.001 |
| 440 | 24.057 | 24.112 | 24.167 | 24.223 | 24.278 | 24.333 | 24.389 | 24.444 | 24.499 | 24.555 |


| $\mathbf{4 5 0}$ | 24.61 | 24.665 | 24.721 | 24.776 | 24.832 | 24.887 | 24.943 | 24.998 | 25.053 | 25.109 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{4 6 0}$ | 25.164 | 25.22 | 25.275 | 25.331 | 25.386 | 25.442 | 25.497 | 25.553 | 25.608 | 25.664 |
| $\mathbf{4 7 0}$ | 25.72 | 25.775 | 25.831 | 25.886 | 25.942 | 25.998 | 26.053 | 26.109 | 26.165 | 26.22 |
| $\mathbf{4 8 0}$ | 26.276 | 26.332 | 26.387 | 26.443 | 26.499 | 26.555 | 26.61 | 26.666 | 26.722 | 26.778 |
| $\mathbf{4 9 0}$ | 26.834 | 26.889 | 26.945 | 27.001 | 27.057 | 27.113 | 27.169 | 27.225 | 27.281 | 27.337 |


| ${ }^{\circ} \mathrm{C}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 500 | 27.393 | 27.449 | 27.505 | 27.561 | 27.617 | 27.673 | 27.729 | 27.785 | 27.841 | 27.897 |
| 510 | 27.953 | 28.010 | 28.066 | 28.122 | 28.178 | 28.234 | 28.291 | 28.347 | 28.403 | 28.460 |
| 520 | 28.516 | 28.572 | 28.629 | 28.685 | 28.741 | 28.798 | 28.854 | 28.911 | 28.967 | 29.024 |
| 530 | 29.080 | 29.137 | 29.194 | 29.250 | 29.307 | 29.363 | 29.420 | 29.477 | 29.534 | 29.590 |
| 540 | 29.647 | 29.704 | 29.761 | 29.818 | 29.874 | 29.931 | 29.988 | 30.045 | 30.102 | 30.159 |
| 550 | 30.216 | 30.273 | 30.330 | 30.387 | 30.444 | 30.502 | 30.559 | 30.616 | 30.673 | 30.730 |
| 560 | 30.788 | 30.845 | 30.902 | 30.960 | 31.017 | 31.074 | 31.132 | 31.189 | 31.247 | 31.304 |
| 570 | 31.362 | 31.419 | 31.477 | 31.535 | 31.592 | 31.650 | 31.708 | 31.766 | 31.823 | 31.881 |
| 580 | 31.939 | 31.997 | 32.055 | 32.113 | 32.171 | 32.229 | 32.287 | 32.345 | 32.403 | 32.461 |
| 590 | 32.519 | 32.577 | 32.636 | 32.694 | 32.752 | 32.810 | 32.869 | 32.927 | 32.985 | 33.044 |
| 600 | 33.102 | 33.161 | 33.219 | 33.278 | 33.337 | 33.395 | 33.454 | 33.513 | 33.571 | 33.630 |
| 610 | 33.689 | 33.748 | 33.807 | 33.866 | 33.925 | 33.984 | 34.043 | 34.102 | 34.161 | 34.220 |
| 620 | 34.279 | 34.338 | 34.397 | 34.457 | 34.516 | 34.575 | 34.635 | 34.694 | 34.754 | 34.813 |
| 630 | 34.873 | 34.932 | 34.992 | 35.051 | 35.111 | 35.171 | 35.230 | 35.290 | 35.350 | 35.410 |
| 640 | 35.470 | 35.530 | 35.590 | 35.650 | 35.710 | 35.770 | 35.830 | 35.890 | 35.950 | 36.010 |
| 650 | 36.071 | 36.131 | 36.191 | 36.252 | 36.312 | 36.373 | 36.433 | 36.494 | 36.554 | 36.615 |
| 660 | 36.675 | 36.736 | 36.797 | 36.858 | 36.918 | 36.979 | 37.040 | 37.101 | 37.162 | 37.223 |
| 670 | 37.284 | 37.345 | 37.406 | 37.467 | 37.528 | 37.590 | 37.651 | 37.712 | 37.773 | 37.835 |
| 680 | 37.896 | 37.958 | 38.019 | 38.081 | 38.142 | 38.204 | 38.265 | 38.327 | 38.389 | 38.450 |
| 690 | 38.512 | 38.574 | 38.636 | 38.698 | 38.760 | 38.822 | 38.884 | 38.946 | 39.008 | 39.070 |
| 700 | 39.132 | 39.194 | 39.256 | 39.318 | 39.381 | 39.443 | 39.505 | 39.568 | 39.630 | 39.693 |
| 710 | 39.755 | 39.818 | 39.880 | 39.943 | 40.005 | 40.068 | 40.131 | 40.193 | 40.256 | 40.319 |
| 720 | 40.382 | 40.445 | 40.508 | 40.570 | 40.633 | 40.696 | 40.759 | 40.822 | 40.886 | 40.949 |
| 730 | 41.012 | 41.075 | 41.138 | 41.201 | 41.265 | 41.328 | 41.391 | 41.455 | 41.518 | 41.581 |
| 740 | 41.645 | 41.708 | 41.772 | 41.835 | 41.899 | 41.962 | 42.026 | 42.090 | 42.153 | 42.217 |
| 750 | 42.281 | 42.344 | 42.408 | 42.472 | 42.536 | 42.599 | 42.663 | 42.727 | 42.791 | 42.855 |
| 760 | 42.919 | 42.983 | 43.047 | 43.111 | 43.175 | 43.239 | 43.303 | 43.367 | 43.431 | 43.495 |
| 770 | 43.559 | 43.624 | 43.688 | 43.752 | 43.817 | 43.881 | 43.945 | 44.010 | 44.074 | 44.139 |
| 780 | 44.203 | 44.267 | 44.332 | 44.396 | 44.461 | 44.525 | 44.590 | 44.655 | 44.719 | 44.784 |
| 790 | 44.848 | 44.913 | 44.977 | 45.042 | 45.107 | 45.171 | 45.236 | 45.301 | 45.365 | 45.430 |
| 800 | 45.494 | 45.559 | 45.624 | 45.688 | 45.753 | 45.818 | 45.882 | 45.947 | 46.011 | 46.076 |
| 810 | 46.141 | 46.205 | 46.270 | 46.334 | 46.399 | 46.464 | 46.528 | 46.593 | 46.657 | 46.722 |
| 820 | 46.786 | 46.851 | 46.915 | 46.980 | 47.044 | 47.109 | 47.173 | 47.238 | 47.302 | 47.367 |
| 830 | 47.431 | 47.495 | 47.560 | 47.624 | 47.688 | 47.753 | 47.817 | 47.881 | 47.946 | 48.010 |
| 840 | 48.074 | 48.138 | 48.202 | 48.267 | 48.331 | 48.395 | 48.459 | 48.523 | 48.587 | 48.651 |
| 850 | 48.715 | 48.779 | 48.843 | 48.907 | 48.971 | 49.034 | 49.098 | 49.162 | 49.226 | 49.290 |
| 860 | 49.353 | 49.417 | 49.481 | 49.544 | 49.608 | 49.672 | 49.735 | 49.799 | 49.862 | 49.926 |
| 870 | 49.989 | 50.052 | 50.116 | 50.179 | 50.243 | 50.306 | 50.369 | 50.432 | 50.495 | 50.559 |
| 880 | 50.622 | 50.685 | 50.748 | 50.811 | 50.874 | 50.937 | 51.000 | 51.063 | 51.126 | 51.188 |
| 890 | 51.251 | 51.314 | 51.377 | 51.439 | 51.502 | 51.565 | 51.627 | 51.690 | 51.752 | 51.815 |
| 900 | 51.877 | 51.940 | 52.002 | 52.064 | 52.127 | 52.189 | 52.251 | 52.314 | 52.376 | 52.438 |
| 910 | 52.500 | 52.562 | 52.624 | 52.686 | 52.748 | 52.810 | 52.872 | 52.934 | 52.996 | 53.057 |
| 920 | 53.119 | 53.181 | 53.243 | 53.304 | 53.366 | 53.427 | 53.489 | 53.550 | 53.612 | 53.673 |


| $\mathbf{9 3 0}$ | 53.735 | 53.796 | 53.857 | 53.919 | 53.980 | 54.041 | 54.102 | 54.164 | 54.225 | 54.286 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{9 4 0}$ | 54.347 | 54.408 | 54.469 | 54.530 | 54.591 | 54.652 | 54.713 | 54.773 | 54.834 | 54.895 |
| $\mathbf{9 5 0}$ | 54.956 | 55.016 | 55.077 | 55.138 | 55.198 | 55.259 | 55.319 | 55.380 | 55.440 | 55.501 |
| $\mathbf{9 6 0}$ | 55.561 | 55.622 | 55.682 | 55.742 | 55.803 | 55.863 | 55.923 | 55.983 | 56.043 | 56.104 |
| $\mathbf{9 7 0}$ | 56.164 | 56.224 | 56.284 | 56.344 | 56.404 | 56.464 | 56.524 | 56.584 | 56.643 | 56.703 |
| $\mathbf{9 8 0}$ | 56.763 | 56.823 | 56.883 | 56.942 | 57.002 | 57.062 | 57.121 | 57.181 | 57.240 | 57.300 |
| $\mathbf{9 9 0}$ | 57.360 | 57.419 | 57.479 | 57.538 | 57.597 | 57.657 | 57.716 | 57.776 | 57.835 | 57.894 |
| ${ }^{\circ} \mathbf{C}$ | $\mathbf{0}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | 5 | 6 | 7 | 8 | $\mathbf{8}$ |
| $\mathbf{1 0 0 0}$ | 57.953 | 58.013 | 58.072 | 58.131 | 58.190 | 58.249 | 58.309 | 58.368 | 58.427 | 58.486 |
| $\mathbf{1 0 1 0}$ | 58.545 | 58.604 | 58.663 | 58.722 | 58.781 | 58.840 | 58.899 | 58.957 | 59.016 | 59.075 |
| $\mathbf{1 0 2 0}$ | 59.134 | 59.193 | 59.252 | 59.310 | 59.369 | 59.428 | 59.487 | 59.545 | 59.604 | 59.663 |
| $\mathbf{1 0 3 0}$ | 59.721 | 59.780 | 59.838 | 59.897 | 59.956 | 60.014 | 60.073 | 60.131 | 60.190 | 60.248 |
| $\mathbf{1 0 4 0}$ | 60.307 | 60.365 | 60.423 | 60.482 | 60.540 | 60.599 | 60.657 | 60.715 | 60.774 | 60.832 |
| $\mathbf{1 0 5 0}$ | 60.890 | 60.949 | 61.007 | 61.065 | 61.123 | 61.182 | 61.240 | 61.298 | 61.356 | 61.415 |
| $\mathbf{1 0 6 0}$ | 61.473 | 61.531 | 61.589 | 61.647 | 61.705 | 61.763 | 61.822 | 61.880 | 61.938 | 61.996 |
| $\mathbf{1 0 7 0}$ | 62.054 | 62.112 | 62.170 | 62.228 | 62.286 | 62.344 | 62.402 | 62.460 | 62.518 | 62.576 |
| $\mathbf{1 0 8 0}$ | 62.634 | 62.692 | 62.750 | 62.808 | 62.866 | 62.924 | 62.982 | 63.040 | 63.098 | 63.156 |
| $\mathbf{1 0 9 0}$ | 63.214 | 63.271 | 63.329 | 63.387 | 63.445 | 63.503 | 63.561 | 63.619 | 63.677 | 63.734 |
| $\mathbf{1 1 0 0}$ | 63.792 | 63.850 | 63.908 | 63.966 | 64.024 | 64.081 | 64.139 | 64.197 | 64.255 | 64.313 |
| $\mathbf{1 1 1 0}$ | 64.370 | 64.428 | 64.486 | 64.544 | 64.602 | 64.659 | 64.717 | 64.775 | 64.833 | 64.890 |
| $\mathbf{1 1 2 0}$ | 64.948 | 65.006 | 65.064 | 65.121 | 65.179 | 65.237 | 65.295 | 65.352 | 65.410 | 65.468 |
| $\mathbf{1 1 3 0}$ | 65.525 | 65.583 | 65.641 | 65.699 | 65.756 | 65.814 | 65.872 | 65.929 | 65.987 | 66.045 |
| $\mathbf{1 1 4 0}$ | 66.102 | 66.160 | 66.218 | 66.275 | 66.333 | 66.391 | 66.448 | 66.506 | 66.564 | 66.621 |
| $\mathbf{1 1 5 0}$ | 66.679 | 66.737 | 66.794 | 66.852 | 66.910 | 66.967 | 67.025 | 67.082 | 67.140 | 67.198 |
| $\mathbf{1 1 6 0}$ | 67.255 | 67.313 | 67.370 | 67.428 | 67.486 | 67.543 | 67.601 | 67.658 | 67.716 | 67.773 |
| $\mathbf{1 1 7 0}$ | 67.831 | 67.888 | 67.946 | 68.003 | 68.061 | 68.119 | 68.176 | 68.234 | 68.291 | 68.348 |
| $\mathbf{1 1 8 0}$ | 68.406 | 68.463 | 68.521 | 68.578 | 68.636 | 68.693 | 68.751 | 68.808 | 68.865 | 68.923 |
| $\mathbf{1 1 9 0}$ | 68.980 | 69.037 | 69.095 | 69.152 | 69.209 | 69.267 | 69.324 | 69.381 | 69.439 | 69.496 |
| $\mathbf{1 2 0 0}$ | 69.553 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |

Table 2. J Type Thermocouple EMF Table for -ve Temperatures (in mV)

| ${ }^{\circ} \mathrm{C}$ | 0 | -1 | -2 | -3 | -4 | -5 | -6 | -7 | -8 | -9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -210 | -8.095 |  |  |  |  |  |  |  |  |  |
| -200 | -7.890 | -7.912 | -7.934 | -7.955 | -7.976 | -7.996 | -8.017 | -8.037 | -8.057 | -8.076 |
| -190 | -7.659 | -7.683 | -7.707 | -7.731 | -7.755 | -7.778 | -7.801 | -7.824 | -7.846 | -7.868 |
| -180 | -7.403 | -7.429 | -7.456 | -7.482 | -7.508 | -7.534 | -7.559 | -7.585 | -7.610 | -7.634 |
| -170 | -7.123 | -7.152 | -7.181 | -7.209 | -7.237 | -7.265 | -7.293 | -7.321 | -7.348 | -7.376 |
| -160 | -6.821 | -6.853 | -6.883 | -6.914 | -6.944 | -6.975 | -7.005 | -7.035 | -7.064 | -7.094 |
| -150 | -6.500 | -6.533 | -6.566 | -6.598 | -6.631 | -6.663 | -6.695 | -6.727 | -6.759 | -6.790 |
| -140 | -6.159 | -6.194 | -6.229 | -6.263 | -6.298 | -6.332 | -6.366 | -6.400 | -6.433 | -6.467 |
| -130 | -5.801 | -5.838 | -5.874 | -5.910 | -5.946 | -5.982 | -6.018 | -6.054 | -6.089 | -6.124 |
| -120 | -5.426 | -5.465 | -5.503 | -5.541 | -5.578 | -5.616 | -5.653 | -5.690 | -5.727 | -5.764 |
| -110 | -5.037 | -5.076 | -5.116 | -5.155 | -5.194 | -5.233 | -5.272 | -5.311 | -5.350 | -5.388 |
| -100 | -4.633 | -4.674 | -4.714 | -4.755 | -4.796 | -4.836 | -4.877 | -4.917 | -4.957 | -4.997 |
| -90 | -4.215 | -4.257 | -4.300 | -4.342 | -4.384 | -4.425 | -4.467 | -4.509 | -4.550 | -4.591 |
| -80 | -3.786 | -3.829 | -3.872 | -3.916 | -3.959 | -4.002 | -4.045 | -4.088 | -4.130 | -4.173 |
| -70 | -3.344 | -3.389 | -3.434 | -3.478 | -3.522 | -3.566 | -3.610 | -3.654 | -3.698 | -3.742 |
| -60 | -2.893 | -2.938 | -2.984 | -3.029 | -3.075 | -3.120 | -3.165 | -3.210 | -3.255 | -3.300 |
| -50 | -2.431 | -2.478 | -2.524 | -2.571 | -2.617 | -2.663 | -2.709 | -2.755 | -2.801 | -2.847 |
| -40 | -1.961 | -2.008 | -2.055 | -2.103 | -2.150 | -2.197 | -2.244 | -2.291 | -2.338 | -2.385 |


| $-\mathbf{3 0}$ | -1.482 | -1.530 | -1.578 | -1.626 | -1.674 | -1.722 | -1.770 | -1.818 | -1.865 | -1.913 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $-\mathbf{2 0}$ | -0.995 | -1.044 | -1.093 | -1.142 | -1.190 | -1.239 | -1.288 | -1.336 | -1.385 | -1.433 |
| $-\mathbf{1 0}$ | -0.501 | -0.550 | -0.600 | -0.650 | -0.699 | -0.749 | -0.798 | -0.847 | -0.896 | -0.946 |
| $\mathbf{0}$ | 0.000 | -0.050 | -0.101 | -0.151 | -0.201 | -0.251 | -0.301 | -0.351 | -0.401 | -0.451 |

Table 3. Polynomial Constants for Different Thermocouples

|  | Type |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{E}$ | $\mathbf{J}$ | $\mathbf{K}$ | $\mathbf{R}$ | $\mathbf{S}$ | $\mathbf{T}$ |
| $\mathbf{a}_{\mathbf{0}}$ | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| $\mathbf{a}_{\mathbf{1}}$ | $1.7057035 \mathrm{E}-2$ | $1.978425 \mathrm{E}-2$ | $2.508355 \mathrm{E}-2$ | $1.8891380 \mathrm{E}-1$ | $1.84949460 \mathrm{E}-1$ | $2.592800 \mathrm{E}-2$ |
| $\mathbf{a}_{\mathbf{2}}$ | $-2.3301759 \mathrm{E}-7$ | $-2.00120204 \mathrm{E}-7$ | $7.860106 \mathrm{E}-8$ | $-9.3835290 \mathrm{E}-5$ | $-8.00504062 \mathrm{E}-5$ | $-7.602961 \mathrm{E}-7$ |
| $\mathbf{a}_{\mathbf{3}}$ | $6.543558 \mathrm{E}-12$ | $1.036969 \mathrm{E}-11$ | $-2.503131 \mathrm{E}-10$ | $1.3068619 \mathrm{E}-7$ | $1.02237430 \mathrm{E}-7$ | $4.637791 \mathrm{E}-11$ |
| $\mathbf{a}_{4}$ | $-7.3562749 \mathrm{E}-17$ | $-2.549687 \mathrm{E}-16$ | $8.315270 \mathrm{E}-14$ | $-2.2703580 \mathrm{E}-10$ | $-1.52248592 \mathrm{E}-10$ | $-2.165394 \mathrm{E}-15$ |
| $\mathbf{a}_{\mathbf{5}}$ | $-1.7896001 \mathrm{E}-21$ | $3.585153 \mathrm{E}-21$ | $-1.228034 \mathrm{E}-17$ | $3.5145659 \mathrm{E}-13$ | $1.88821343 \mathrm{E}-13$ | $6.048144 \mathrm{E}-20$ |
| $\mathbf{a}_{6}$ | $8.4036165 \mathrm{E}-26$ | $-5.344285 \mathrm{E}-26$ | $9.804036 \mathrm{E}-22$ | $-3.8953900 \mathrm{E}-16$ | $-1.59085941 \mathrm{E}-16$ | $-7.293422 \mathrm{E}-25$ |
| $\mathbf{a}_{\mathbf{7}}$ | $-1.3735879 \mathrm{E}-30$ | $5.099890 \mathrm{E}-31$ | $-4.413030 \mathrm{E}-26$ | $2.8239471 \mathrm{E}-19$ | $8.23027880 \mathrm{E}-20$ |  |
| $\mathbf{a}_{\mathbf{8}}$ | $1.0629823 \mathrm{E}-35$ |  | $1.057734 \mathrm{E}-30$ | $-1.2607281 \mathrm{E}-22$ | $-2.34181944 \mathrm{E}-23$ |  |
| $\mathbf{a}_{\mathbf{9}}$ | $-3.2447087 \mathrm{E}-41$ |  | $-1.052755 \mathrm{E}-35$ | $3.1353611 \mathrm{E}-26$ | $2.79786260 \mathrm{E}-27$ |  |
| $\mathbf{a}_{\mathbf{1 0}}$ |  |  |  | $-3.3187769 \mathrm{E}-30$ |  |  |

Table 4. Test Results

| Input | Compensated | Expected | Actual | Error | Error on FS |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{m V}$ | $\mathbf{m V}$ | Reading | Reading | ${ }^{\circ} \mathbf{C}$ | $\%$ |
|  |  |  |  |  |  |
| -7.90 | -6.42 | -148 | -147 | -1 | 0.08 |
| -4.63 | -3.15 | -66 | -67 | 1 | -0.08 |
| 0.00 | 1.49 | 29 | 29 | 0 | 0.00 |
| 5.27 | 6.75 | 127 | 127 | 0 | 0.00 |
| 10.78 | 12.26 | 227 | 228 | -1 | 0.08 |
| 16.33 | 17.81 | 328 | 328 | 0 | 0.00 |
| 21.85 | 23.33 | 427 | 428 | -1 | 0.08 |
| 27.39 | 28.88 | 526 | 525 | 1 | -0.08 |
| 33.10 | 34.59 | 625 | 625 | 0 | 0.00 |
| 39.13 | 40.62 | 724 | 724 | 0 | 0.00 |
| 45.49 | 46.98 | 824 | 824 | 0 | 0.00 |
| 51.88 | 53.36 | 924 | 924 | 0 | 0.00 |
| 57.95 | 59.44 | 1027 | 1025 | 2 | -0.17 |
| 63.79 | 65.28 | 1126 | 1124 | 2 | -0.17 |
| 66.68 | 68.16 | 1176 | 1175 | 1 | -0.08 |

## Max Error $=2^{\circ} \mathrm{C}$

Test Condition:
Room Temperature $=29^{\circ} \mathrm{C}$
Cold Junction Compensation $=1.49 \mathrm{mV}$

